Attachment B-2

Sedflume Erosion Data and Analysis

The Conowingo Reservoir sediment bed is composed of cohesive sediments. Non-cohesive sediment (sand and gravel) erosion and settling can be generally estimated from grain size distribution and mineral density. Cohesive sediment transport processes are dominated by other factors. Cohesive sediments are generally a mixture of sand, silt, and clay sized particles.

A general definition for cohesive sediment is sediment for which the erosion rate cannot be estimated by standard sand/gravel transport methods. In these cases, cohesive forces are equivalent to or are greater than the gravitational forces that dominate sand transport. Cohesive sediment erosion characteristics are highly dependent upon factors such as particle size distribution, particle coatings, fine sediment mineralogy, organic content, bulk density, gas content, pore-water chemistry, and biological activity. Erosion rate and critical shear stress for erosion can vary significantly with small changes in only one of these interdependent parameters. It has been well demonstrated that critical stress and erosion rates for cohesive sediment can vary over several orders of magnitude for sediments with only slightly differing properties. Therefore, the influence of cohesion on sediment processes is significant. Qualitatively, it is understood which properties most significantly influence erosion. However, there are no quantitative methods available to determine erosion rate from cohesive sediment properties. Therefore, due to the sensitivity and wide range of influencing parameters, erosion characteristics of cohesive sediments are determined by site-specific analysis of erosion with erosion flumes.

Several flumes are available to parameterize site-specific cohesive sediment erosion algorithms. Most of these devices operate over a range of low shear stress (<2 Pa) and are consequently capable of measuring only surface sediment erosion. Sedflume is an erosion device with capability to impose bed stresses in the range of 0.1 to 12 Pa and measures erosion rates from sediment cores taken from the field (for in-situ or stratified bed conditions) or prepared in the laboratory (for assessing disturbed sediments such as dredged material). Sedflume is designed to quantify erosion rates for surface and sub-surface sediments. These measurements permit description of the vertical variation of erosion rate within the bed. It should be noted that even if sediments are well mixed, cohesive sediment bed erosion will change with depth due to the influence of consolidation (bed density) on erosion rate. Erosion rate can vary by several orders of magnitude between surficial sediments and sediment buried less than 30 cm below the surface. Sedflume was selected to quantify erosion rate variation with depth (density) for this study.

Methods

This section describes the field experiments, sampling and experimental methods, and data analysis methods used in determining cohesive sediment erosion within Conowingo Reservoir. Background and technical information about the experimental device is presented first, followed by description of how these devices were deployed during field experiments to meet the study objectives.



Figure 1. Sedflume erosion flume (lower right). Core inserted into test section (upper left). Core surface flush with bottom of flow channel (upper right). Table of shear stress associated with channel flow rates (lower left).

Sedflume

Sedflume is a field- or laboratory-deployable flume for quantifying cohesive sediment erosion. The USACE-developed Sedflume is a derivative of the flume developed by researchers at the University of California at Santa Barbara (McNeil et al. 1996). The flume includes an 80-cm-long inlet section (Figure 1) with cross-sectional area of 2×10 cm for uniform, fully developed, smooth-turbulent flow. The inlet section is followed by a 15-cm-long test section with a 10×15 cm open bottom (the open bottom can accept cores with rectangular cross-section (10×15 cm) or circular cross-section (10-cm diameter)). Coring tubes and flume test section, inlet section, and exit sections are constructed of clear polycarbonate materials to permit observation of sediment-water interactions during the course of erosion experiments. The flume includes a port over the test section to provide access to the core surface for physical sampling. The flume accepts sediment cores up to 80-cm in length.

Erosion Experiments

Prior to the erosion experiment, descriptions of the core are recorded, including length, condition of the core surface, biological activity, and any visual evidence of layering. Cores are inserted into the testing section of Sedflume and a screw jack is used to advance the plunger such that the core surface becomes flush with the bottom wall of the flume. Flow is directed over the sample by diverting flow from a 3-hp pump, through a 5-cm inner diameter hose, into the flume. The flow through the flume produces shear stress on the surface of the core. (Numerical, experimental, and analytical analyses have been performed to relate flowrate to bottom shear stress.) Erosion of the surface sediment is initiated as the shear stress is increased beyond the critical stress for erosion, τ_{cr} . As sediment erodes from the core surface, the operator advances the screw jack to maintain the sediment surface flush with the bottom wall of the erosion flume. Figure 1 includes a photograph of the flume, a close-up photograph of the test section, and a table of flow rate/shear stress relationships.

Erosion rate is determined from the displacement of the core surface over the elapsed time of the experiment. Generally, erosion experiments are performed in repeating sequences of increasing shear stress. Operator experience permits sequencing of erosion tests to allow greater vertical resolution of shear stress/erosion rate data where required. The duration of each erosion experiment at a specified shear stress is dependent on the rate of erosion and generally is between 0.25 and 15 minutes. Shear stresses that induce no measurable erosion are also recorded. The range of shear stress for each cycle is determined by the operator based on the previous erosion sequences and erosion behavior during the ongoing sequence.

Sediment Bulk Properties

Physical samples for bulk sediment property measurements are taken at approximately 3-5 cm intervals during erosion experiments, generally at the end of each shear stress cycle. Physical samples are collected by draining the flume channel, opening the port over the test section, and extracting a sample from the sediment bed. Properties measured include bulk density and grain-size distribution, and separate samples were collected from the core surface for these analyses. These properties strongly influence erosion; therefore, understanding their variation with depth is important in interpreting the erosion data.

<u>Bulk Density Measurements.</u> Bulk sediment density of physical samples is determined by a wet-dry weight analysis. Physical samples are extracted from the saturated core surface and placed in a pre-weighed aluminum tray. Sample weight is recorded immediately after collection and again after a minimum of 12 hours in an 90° C (194° F) drying oven. Wet weight of the sample was calculated by subtracting tare weight from the weight of the sample. The dry weight of the sample was calculated as the tare weight subtracted from the weight after drying. The water content w is then given

$$w = \begin{cases} \frac{m_w \uparrow m_d}{m_d} \end{cases}$$
(1)

where m_W and m_d are the wet and dry weights, respectively. A volume of saturated sed- iment, V, consists of both solid particles and water and can be written as

$$V = V_s + V_w \tag{2}$$

where V_S is the volume of solid particles and V_W is the volume of water. If the sediment particles and water have density s and w, respectively, the water content of the sediment can be written as

$$w = \frac{\sum_{w} V_{w}}{\sum_{s} V_{s}}$$
(3)

A mass balance of the volume of sediment gives

$$\rangle V = \rangle_s V_s + \rangle_w V_w \tag{4}$$

where \rangle is the bulk density of the sediment sample.

(1)-(4) are used to derive an explicit expression for the bulk density of the sediment sample, \rangle , as a function of the water content, *w*, and the densities of the sediment particles and water. This equation is

$$\rangle = \rangle_{s} + \frac{w_{\delta}(\langle \rangle_{w} \downarrow \rangle_{s})}{\rangle_{w} + w_{\delta}}$$
(5)

For the purpose of these calculations, $\rangle_s = 2.65 \text{ g} \cdot \text{cm}^{-3}$ and \rangle_w is calculated for measured pore water at sample temperature.

<u>Particle-Size Distribution.</u> Samples collected during erosion experiments were transported to the Sediment Transport Processes Lab at ERDC for grain size analysis. A Beckman-Coulter LS 13-320 laser particle-sizer was used to measure the particle-size distributions in sub-samples collected from the cores. The LS 13-320 measures particle size over the range 0.4 to 900 µm. Particle size distributions were measured by first removing and sieving particles larger than 850 µm. The passing portion of the sample was added to a small volume of water (approximately 150 mL) and sonicated using a high-powered laboratory sonicator to disperse the sediment. The dispersed solution was placed in the particle sizer fluid module. The sample is pumped and recirculated through the optical module. The optical module includes a spatial filter assembly containing a laser diode and laser beam collimator. The diffraction detector assembly contains a custom photodetector array that is used for the measurement of light scattering by the suspended particles. The distribution of grain sizes and median grain sizes is derived from this light scattering measurement. The size distribution of fines passing the 850 µm sieve is scaled to account for the sediment mass retained on the sieve. Organic material was not oxidized before grain size analysis was performed; therefore grain size distributions include organic material.

Multivariate Erosion Rate Prediction

The goal of erosion data analysis is to determine appropriate parameterization of erosion processes for numerical modeling studies. For this study, the erosion data are to be described in the SEDZLJ model. SEDZLJ is flexible in the form of the erosion equation, and the effects of bulk density, depth, and applied shear stress may be represented as indicated by the erosion data. Analysis of the erosion data from Conowingo Reservoir suggested that the erosion algorithm should be of the following form:

$$E = 0; \qquad (| < |_{c}$$

$$E = A |^{n}; \qquad) \qquad (|_{c} < | < |_{m}$$

$$E = A |^{n}_{m}; \qquad (| > |_{m})$$
(6)

where *E* represents erosion rate (cm·s⁻¹) from the bed, τ is bed shear stress, τ_c is critical stress for erosion, *A* is an empirical constant, *n* is an empirical exponent, and τ_m is bed stress at which erosion rate becomes constant. Solution of Equation (6) to data requires solving for three parameters, τ_c , *A*, and *n*. Bed stress for the upper limit of erosion rate is determined by examining the data. The best fit of Equation (6) to measured data is accomplished through an iterative, multi-parameter, least-squares method on the linear transform of Equation (6).

Field Experiments

Field experiments were conducted from April 11 through April 16 of 2012. Field experiments included core collection, physical sampling, and cohesive sediment erosion experiments.

Core Collection

On April 11, 2012, eight 10-cm (4-inch) diameter cores were collected from eight locations (Figure 2, Table 1) within Conowingo Reservoir for the purpose of erosion experiments. The eight core collection locations were provided to ERDC by the United State Geological Survey (USGS), in Maryland State Plane North American Datum (NAD) 83 northing and easting. A gravity corer was used to collect a core from each location.

Table 1. Core Summary										
Core ID	Northing	Easting	Collection Method	Collection Date	Sample Depth (cm below sediment sur- face)					
Station 1	728720	1541780	Gravity	11 April 2012	20					
Station 2	737040	1535500	Gravity	11 April 2012	36					
Station 3	735660	1534110	Gravity	11 April 2012	26.5					
Station 4	743790	1530280	Gravity	11 April 2012	18					
Station 5	743520	1528760	Gravity	11 April 2012	30.5					
Station 6	757140	1527370	Gravity	11 April 2012	19.5					
Station 9	766460	1518910	Gravity	11 April 2012	17.5					
Station 10	772540	1514680	Gravity	11 April 2012	19.5					

The ERDC gravity corer (Figure 3A) is constructed of steel and weighs approximately 32 kg (70 lbs). The gravity corer consists of a core barrel, check valve, fins, and cable harness. The gravity corer is lowered to the bottom and penetrates the bed by its own weight and momentum. The check valve serves to create a seal above the core to prevent the captured sediment core from slipping out of the core tube. Once the core is retrieved to the vessel, a plunger with Bentonite paste (for sealing and lubrication) is inserted into the bottom of the core and each end of the core is sealed with end caps (Figures 3B-C). Each core was labeled, logged, and stored submerged in water on the vessel deck.



Figure 2. Coring locations in Conowingo Reservoir, MD.

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B) Plungers with Bentonite paste



A) Gravity Corer

C) Core with plunger in

Erosion Experiments

Cores collected were transported by vessel to the ERDC-CHL Field Sediment Laboratory (located on Conowingo Reservoir at the Glen Cove Marina site). Erosion experiments were conducted 13 April through 16 April 2012, in the field laboratory following the Sedflume methods presented earlier in this report. During the time of erosion experiments, sediment cores were stored in a shaded barrel, filled with site water.

Results and Discussion

Cohesive sediment transport process data collected during the field study were analyzed to determine SEDZLJ model parameterizations for cohesive sediment erosion and settling velocity. This section presents results of the data analysis, model parameterization, and general observation with discussion. This

report presents physical descriptions of each core including:, bed density profiles, grain size analysis, and erosion analysis of each core, including definition of bed layers that erode similarly.

Cohesive Sediment Erosion

Analysis of cohesive sediment erosion data obtained from undisturbed field cores is inherently complex. Cohesive sediment erosion is sensitive to slight changes in bed density, deposit mineralogy, gas content, organic content, biological activity, debris and a host of other factors. In many cases, these factors change significantly at relatively small vertical scales (such as depositional bed sequences). Consequently, measured cohesive sediment erosion rates from field cores are notoriously variable. To compensate for the large variance in measured erosion rates, field erosion experiments are conducted in a manner to produce a large sample from which to derive statistically representative relationships for various numerical erosion algorithms. To ensure high quality in the data analysis, data and associated experimental notes are evaluated to identify outliers in the dataset. Outliers are rejected based on comparisons between adjacent data points and experimental log notes.

Cores 1-5 (from the downstream half of the reservoir) were composed primarily of silt and clay and the sediment composition was fairly uniform with depth aside from the occasional increase in leafy organic matter or the occasional sand lens. Sand content generally increased upstream of Core 6 and sediment composition became more variable with depth. The composition of Core 10 was highly variable with depth, with as much as 80% sand content.

Erosion Parameterization

Erosion rate data were evaluated for relationships between erosion rate, bed density, and applied shear stress. In general, the erosion behavior of the cores gradually varied with depth. The occasional sand lens or change in organic content occasionally produced distinctly different erosion behavior. The erosion data were grouped in layers to account for the changing critical erosion depth and erosion rates with depth.

The erosion data from Core 1 will be presented here to illustrate the parameterization of the erosion data from Conowingo Reservoir. The composition of Core 1 was very uniform and was predominantly silt (80-85% silt from the physical samples). Figure 3 presents the erosion data with depth. First, the erosion data were grouped vertically within cores. This grouping was accomplished by reviewing the erosion notes and erosion rate relationships to depth, density, and shear stress. At the sediment water interface, there is typically a thin, low-density layer that erodes more easily than the more highly consolidated sediments deeper in the sediment bed. This was observed for Core 1 between depths of 0 - 4 cm into the core with a critical shear stress of 0.2 Pa, which is defined as Layer Core01_L1. Beneath the surface layer was a layer from 5 - 10 cm that had a critical shear stress of 0.4 Pa, and reduced erosion rate associated with the increase in bed density with depth into the core. Core01_L3 (10-14 cm depth) was associated with an increase in critical shear stress to 0.8 Pa and further reduction of erosion rates with depth into the core.



Figure 3. Erosion rate data of Core 1. For erosion rate data set, colors indicate the layers of the core as inferred from erosion data visual observations and physical properties

A multivariate, least-squares fit of erosion rate to shear stress for the standard form of the Partheniades erosion equation (Core 01, Layer 2) is presented in the upper plot of Figure 4. In the bottom plot of Figure 4, a parameterization of the piece-wise linear form of the Partheniades implementation in HEC-RAS is presented. Erosion parameterization for each layer in each core is provided in Table 2 (Full Partheniades) and Table 3 (HEC-RAS Partheniades). For instances where the range of erosion measurements was nearly linear, the second limb of the HEC-RAS parameterization is not provided.



Figure 4. Erosion parameterization for Core 1, Layer 2. (Upper) best-fit line to Partheniades' erosion

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All cores collected exhibited cohesive erosion behavior. Critical shear stress for erosion generally increased with depth and erosion rates at a given shear stress decreased with depth. These are common observations associated with stronger bonding with increased sediment consolidation and density.

Table 2. Cohesive Sediment Erosion Parameterization								
	Critical Shear (τ _{cr})		Erosion Rate Con- stant (M)	Erosion Rate Ex- ponent (n)				
Layer ID	Depth (cm)	Ра	-	-				
Core01_L1	0-4	0.20	2.02E-02	1.14				
Core01_L2	5-10	0.40	2.89E-02	1.10				
Core01_L3	10-14	0.80	3.52E-02	0.96				
Core02_L1	0-10	0.20	1.01E-01	1.05				
Core02_L2	10-17	0.40	5.98E-02	1.52				
Core02_L3	17-24	0.80	3.73E-02	1.36				
Core02_L4	24-32	1.60	9.18E-02	0.92				
Core02_L3&4	17-32	0.80	3.86E-02	0.92				
Core03_L1	0-2.5	0.20	9.90E-03	0.98				
Core03_L2	2.5-22	0.80	8.08E-02	1.00				
Core04_L1	0-2	0.20	1.04E-02	1.21				
Core04_L2	2-11	0.80	3.23E-02	0.90				

Table 2. Cohesive Sediment Erosion Parameterization									
		Critical Shear (τ _{cr})	Erosion Rate Con- stant (M)	Erosion Rate Ex- ponent (n)					
Layer ID	Depth (cm)	Ра	-	-					
Core05_L1	0-5	0.20	1.20E-02	1.04					
Core05_L2	5-12	0.78	2.17E-02	1.37					
Core05_L3	12-24	1.60	9.80E-02	0.99					
Core06_L1	0-2	0.10	1.48E-02	0.90					
Core06_L2	2-14	1.60	3.31E-02	1.04					
Core09_L1	0-2	0.20	8.20E-03	1.41					
Core09_L2	2-9	1.52	2.32E-02	1.36					
Core10_L1	0-8	0.18	3.40E-02	1.31					
Core10_L2	8-16	1.14	1.70E-02	1.61					

Table 3. Cohesive Sediment Erosion Parameterization for HEC-RAS										
	Depth	Shear Thresh- old		Erosio	Erosion Rate		s Wasting reshold	Mass Wasting Rate		
Layer ID	(cm)	Ра	lb/ft2	kg/m2/s	lb/ft2/hr	Ра	lb/ft2	kg/m2/s	lb/ft2/hr	
Core01_L1	0-4	0.2	0.0042	2.02E-02	14.9	1	0.0209	0.263	193.9099	
Core01_L2	5-10	0.4	0.0084	3.24E-02	23.9	-	-	-	-	
Core01_L3	10-14	0.8	0.0167	3.39E-02	25.0	-	-	-	-	
Core02_L1	0-10	0.2	0.0042	1.04E-01	76.7	-	-	-	-	
Core02_L2	10-17	0.4	0.0084	6.32E-02	46.6	0.9	0.0188	0.323	238	
Core02_L3	17-24	0.8	0.0167	4.62E-02	34.1	-	-	-	-	
Core02_L4	24-32	1.6	0.0334	8.86E-02	65.3	-	-	-	-	
Core02_L3&4	17-32	0.8	0.0167	3.53E-02	26.0	-	-	-	-	
Core03_L1	0-2.5	0.2	0.0042	9.60E-03	7.08	-	-	-	-	
Core03_L2	2.5-22	0.8	0.0167	8.07E-02	59.5	-	-	-	-	
Core03_L1&2	0-22	0.2	0.0042	1.09E-02	8.04	2	0.0418	0.237	175	
Core04_L1	0-2	0.2	0.0042	1.20E-02	8.85	0.8	0.0167	0.087	64.1	
Core04_L2	2-11	0.8	0.0167	2.82E-02	20.8	-	-	-	-	
Core05_L1	0-5	0.2	0.0042	1.28E-02	9.44	-	-	-	-	
Core05_L2	5-12	0.8	0.0167	2.22E-02	16.4	2	0.0418	0.125	92.2	

Table 3. Cohesive Sediment Erosion Parameterization for HEC-RAS										
	Depth (cm)	Shear Thresh- old		Erosion Rate		Mass Wasting Threshold		Mass Wasting Rate		
Layer ID		Ра	lb/ft2	kg/m2/s	lb/ft2/hr	Ра	lb/ft2	kg/m2/s	lb/ft2/hr	
Core05_L3	12-24	1.6	0.0334	9.76E-02	72.0	-	-	-	-	
Core06_L1	0-2	0.1	0.0021	1.32E-02	9.73	-	-	-	-	
Core06_L2	2-14	1.59	0.0332	3.41E-02	25.1	-	-	-	-	
Core09_L1	0-2	0.2	0.0042	1.25E-02	9.22	0.8	0.0167	0.102	75.2	
Core09_L2	2-9	1.58	0.033	3.43E-02	25.3	-	-	-	-	
Core10_L1	0-8	0.19	0.004	5.08E-02	37.5	-	-	-	-	
Core10_L2	8-16	1.19	0.0249	1.95E-02	14.4	2.8	0.0585	0.139	102	

Summary

United States Army Corp of Engineers, Baltimore District commissioned the ERDC to conduct cohesive sediment erosion testing services for the purpose of defining erosion rates of reservoir bottom sediments at Conowingo Reservoir, Maryland. ERDC-CHL conducted the erosion testing in April 2012.

Eight, 4-inch (10-cm) diameter sediment cores were collected from the locations throughout Conowingo Reservoir. The cores were eroded in the Field Sediment Transport Laboratory that was operated at the Glen Cove Marina. During erosion experiments, the cores were visually described, eroded, and subsampled for physical properties. Erosion data were analyzed by the layers evident in each core and later grouped by core layers that demonstrated similar erosion characteristics. Empirical coefficients were determined for modeling cohesive sediment bed erosion for individual core layers and groups of core layers that had similar erosion behavior.

Acknowledgements

Mr. Michael Langland from the United States Geological Survey (USGS) provided background information on Conowingo Reservoir and recommended sediment sampling locations for the field data collection and analysis. Mr. Mike and Tommy Kirklin (contractors for USACE-CHL) assisted with core collection, erosion experiments, and sample analysis.

References

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Core Physical Properties



Figure A-1a. Core 1 Surface Photograph, Sample 1.



Figure A-1b. Core 1 Surface Photograph, Sample 2.



Figure A-1c. Core 1 Surface Photograph, Sample 3.



Figure A-1d. Core 1 Surface Photograph, Sample 4.



Figure A-1e. Core 1 Surface Photograph, Sample 5.

Table A-1b. Physical Sample Properties (Core 1)										
Sample	Depth (cm below surf)	Bulk den- sity (g/cm³)	D10(µm)	D50(µm)	D90(µm)	Percent Sand	Percent Silt	Percent Clay		
Surface	0.00	-	5.08	18.33	74.94	14.10	80.33	5.57		
1	0.98	1.28	4.79	15.89	53.64	8.62	85.29	6.09		
2	4.25	1.32	4.89	16.22	55.10	9.11	84.99	5.90		
3	8.10	1.33	4.46	14.91	59.10	10.12	82.76	7.13		
4	11.83	1.33	4.00	13.10	44.72	6.45	84.63	8.92		
5	16.15	1.33	4.44	14.74	53.76	8.88	83.94	7.18		



Susquehanna, Core 1 Surface

Figure A-2a. Grain Size Distribution for Core 1, Physical Sample.

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Susquehanna, Core 1 Sample 1



Figure A-2b. Grain Size Distribution for Core 1, Physical Sample.

Susquehanna, Core 1 Sample 2



Figure A-2c. Grain Size Distribution for Core 1, Physical Sample.



Figure A-2d. Grain Size Distribution for Core 1, Physical Sample.



Figure A-2e. Grain Size Distribution for Core 1, Physical Sample.



Figure A-2f. Grain Size Distribution for Core 1, Physical Sample.

Table A-2b. Physical Sample Properties (Core 2c)										
	Depth	Bulk den-								
	(cm below	sity				Percent	Percent	Percent		
Sample	surf)	(g/cm ³)	D10(µm)	D50(µm)	D90(µm)	Sand	Silt	Clay		
Surface	0.00	-	9.24	218.00	787.16	63.38	34.45	2.17		
1	1.05	1.42	10.64	294.46	934.12	69.76	28.36	1.88		
2	4.95	1.62	111.06	545.72	1113.57	95.84	3.95	0.20		
3	9.63	1.67	7.71	70.78	589.44	52.74	44.44	2.83		
4	13.80	1.38	5.73	23.96	98.95	21.78	73.66	4.56		
5	17.30	1.30	5.72	20.25	78.32	15.36	80.31	4.33		
6	20.80	1.39	6.00	24.57	103.06	22.36	73.56	4.08		
7	25.80	1.38	5.62	22.32	96.57	19.99	75.40	4.62		
8	30.60	1.44	6.61	26.44	115.64	24.59	72.17	3.24		
9	32.63	1.43	5.27	21.99	96.87	19.85	74.85	5.31		

Susquehanna, Core 2c Surface



Figure A-4a. Grain Size Distribution for Core 2c, Physical Sample.



Susquehanna, Core 2c Sample 1

Figure A-4b. Grain Size Distribution for Core 2c, Physical Sample.



Figure A-4c. Grain Size Distribution for Core 2c, Physical Sample.



Susquehanna, Core 2c Sample 3

Figure A-4d. Grain Size Distribution for Core 2c, Physical Sample.



Figure A-4e. Grain Size Distribution for Core 2c, Physical Sample.



Figure A-4f. Grain Size Distribution for Core 2c, Physical Sample.

Susquehanna, Core 2c Sample 6



Figure A-4g. Grain Size Distribution for Core 2c, Physical Sample.



Susquehanna, Core 2c Sample 7

Figure A-4h. Grain Size Distribution for Core 2c, Physical Sample.



Susquehanna, Core 2c Sample 8

Figure A-4i. Grain Size Distribution for Core 2c, Physical Sample.

Susquehanna, Core 2c Sample 9



Figure A-4j. Grain Size Distribution for Core 2c, Physical Sample.

Table A-3b. Physical Sample Properties (Core 3)									
	Depth (cm	Bulk den-							
	below	sity				Percent	Percent	Percent	
Sample	surf)	(g/cm ³)	D10(µm)	D50(µm)	D90(µm)	Sand	Silt	Clay	
	0.00	-	5.43	21.43	103.07	19.98	75.10	4.92	
Surface									
	0.90	1.29	5.97	21.97	101.41	19.43	76.69	3.89	
1									
	4.30	1.34	5.29	20.23	97.87	18.73	76.17	5.09	
2									
	8.98	1.36	5.20	16.86	62.54	11.00	84.01	4.99	
3									
	13.40	1.35	4.70	18.65	167.89	24.05	69.55	6.39	
4									
	18.35	1.36	5.62	26.92	192.94	31.32	64.01	4.67	
5									
	23.00	1.36	5.52	23.48	155.38	26.53	68.84	4.63	
6									


Figure A-6a. Grain Size Distribution for Core 3, Physical Sample.





Figure A-6b. Grain Size Distribution for Core 3, Physical Sample.

Susquehanna, Core 3 Sample 2



Figure A-6c. Grain Size Distribution for Core 3, Physical Sample.

Susquehanna, Core 3 Sample 3



Figure A-6d. Grain Size Distribution for Core 3, Physical Sample.

Susquehanna, Core 3 Sample 4



Figure A-6e. Grain Size Distribution for Core 3, Physical Sample.

Susquehanna, Core 3 Sample 5



Figure A-6f. Grain Size Distribution for Core 3, Physical Sample.

Susquehanna, Core 3 Sample 6



Figure A-6g. Grain Size Distribution for Core 3, Physical Sample.

Table A-4b. Physical Sample Properties (Core 4)										
Sample	Depth (cm below surf)	Bulk den- sity (g/cm ³)	D10(µm)	D50(µm)	D90(µm)	Percent Sand	Percent Silt	Percent Clay		
Surface	0.00	-	5.57	21.01	85.43	17.29	78.03	4.69		
1	0.88	1.43	5.56	29.41	98.38	24.59	70.36	5.05		
2	4.05	1.33	4.97	20.55	124.06	21.77	72.33	5.90		
3	8.55	1.40	4.67	15.82	56.06	9.37	84.13	6.50		
4	13.10	1.46	4.34	15.84	68.63	12.43	79.99	7.58		

Susquehanna, Core 4 Surface



Figure A-8a. Grain Size Distribution for Core 4, Physical Sample.

Susquehanna, Core 4 Sample 1



Figure A-8b. Grain Size Distribution for Core 4, Physical Sample.

Susquehanna, Core 4 Sample 2



Figure A-8c. Grain Size Distribution for Core 4, Physical Sample.

Susquehanna, Core 4 Sample 3



Figure A-8d. Grain Size Distribution for Core 4, Physical Sample.

Susquehanna, Core 4 Sample 4



Figure A-8e. Grain Size Distribution for Core 4, Physical Sample.

Table A-4b. Physical Sample Properties (Core 5)									
	Depth (cm	Bulk den-							
	below	sity				Percent	Percent	Percent	
Sample	surf)	(g/cm ³)	D10(µm)	D50(µm)	D90(µm)	Sand	Silt	Clay	
	0.00	-	5.91	26.01	219.90	30.47	65.35	4.17	
Surface									
	1.10	1.41	6.48	32.47	331.62	37.28	59.38	3.35	
1									
	5.08	1.31	5.76	25.21	140.55	27.60	68.10	4.30	
2									
	8.60	1.37	5.34	21.69	107.11	21.46	73.45	5.09	
3									
	14.60	1.38	5.38	20.38	79.11	16.31	78.71	4.99	
4									
	19.73	1.35	5.60	21.13	83.03	17.30	78.08	4.62	
5									
	23.90	1.36	5.99	22.61	82.48	17.66	78.32	4.02	
6									



Figure A-10a. Grain Size Distribution for Core 5, Physical Sample.

Susquehanna, Core 5 Sample 1



Figure A-10b. Grain Size Distribution for Core 5, Physical Sample.

Susquehanna, Core 5 Sample 2



Figure A-10c. Grain Size Distribution for Core 5, Physical Sample.

Susquehanna, Core 5 Sample 3



Figure A-10d. Grain Size Distribution for Core 5, Physical Sample.

Susquehanna, Core 5 Sample 4



Figure A-10e. Grain Size Distribution for Core 5, Physical Sample.

Susquehanna, Core 5 Sample 5



Figure A-10f. Grain Size Distribution for Core 5, Physical Sample.

Susquehanna, Core 5 Sample 6



Figure A-10g. Grain Size Distribution for Core 5, Physical Sample.

Table A-6b. Physical Sample Properties (Core 6)										
Sample	Depth (cm below surf)	Bulk den- sity (g/cm ³)	D10(µm)	D50(µm)	D90(µm)	Percent Sand	Percent Silt	Percent Clay		
Surface	0.00	-	7.82	159.13	450.74	56.59	40.68	2.74		
1	1.60	1.53	4.41	19.90	197.12	24.45	68.07	7.48		
2	5.43	1.46	4.72	22.68	124.51	25.69	67.79	6.52		
3	10.25	1.52	5.62	30.94	156.51	32.98	62.15	4.87		
4	13.95	1.57	5.62	30.73	168.99	34.46	60.79	4.75		



Figure A-12a. Grain Size Distribution for Core 6, Physical Sample.

Susquehanna, Core 6 Sample 1



Figure A-12b. Grain Size Distribution for Core 6, Physical Sample.

Susquehanna, Core 6 Sample 2



Figure A-12c. Grain Size Distribution for Core 6, Physical Sample.

Susquehanna, Core 6 Sample 3



Figure A-12d. Grain Size Distribution for Core 6, Physical Sample.

Susquehanna, Core 6 Sample 4



Figure A-12e. Grain Size Distribution for Core 6, Physical Sample.

Table A-7b. Physical Sample Properties (Core 9)										
	Depth	Bulk den-								
	(cm below	sity				Percent	Percent	Percent		
Sample	surf)	(g/cm ³)	D10(µm)	D50(µm)	D90(µm)	Sand	Silt	Clay		
	0.00	-	4.73	22.48	105.09	22.58	70.87	6.54		
Surface										
	1.18	1.54	3.91	14.93	66.79	12.04	78.60	9.36		
1										
	1.95	1.55	4.01	14.69	58.43	9.98	81.14	8.88		
2										
	5.20	1.53	3.43	13.02	61.23	10.65	77.29	12.05		
3										
	9.60	1.55	4.22	17.97	83.25	16.57	75.35	8.08		
4										



Figure A-14a. Grain Size Distribution for Core 9, Physical Sample.

Susquehanna, Core 9 Sample 1



Figure A-14b. Grain Size Distribution for Core 9, Physical Sample.

Susquehanna, Core 9 Sample 2



Figure A-14c. Grain Size Distribution for Core 9, Physical Sample.

Susquehanna, Core 9 Sample 3



Figure A-14d. Grain Size Distribution for Core 9, Physical Sample.

Susquehanna, Core 9 Sample 4



Figure A-14e. Grain Size Distribution for Core 9, Physical Sample.

Table A-8b. Physical Sample Properties (Core 10)										
Sample	Depth (cm below surf)	Bulk density (g/cm³)	D10(µm)	D50(µm)	D90(µm)	Percent Sand	Percent Silt	Percent Clay		
Surface	0.00	-	7.92	53.53	382.76	47.76	49.52	2.72		
1	0.73	1.67	10.07	118.55	536.26	64.75	33.01	2.24		
2	5.20	1.77	17.57	300.76	725.76	80.06	18.40	1.54		
3	8.15	1.40	5.35	26.99	234.51	30.70	64.07	5.23		
4	12.00	1.47	4.91	21.67	97.31	20.22	73.67	6.11		
5	15.55	1.53	4.79	23.31	120.45	24.24	69.23	6.53		

Susquehanna, Core 10 Surface



Figure A-15a. Grain Size Distribution for Core 10, Physical Sample.

Susquehanna, Core 10 Sample 1



Figure A-15b. Grain Size Distribution for Core 10, Physical Sample.


Susquehanna, Core 10 Sample 2

Figure A-15c. Grain Size Distribution for Core 10, Physical Sample.



Susquehanna, Core 10 Sample 3

Figure A-15d. Grain Size Distribution for Core 10, Physical Sample.

Susquehanna, Core 10 Sample 4



Figure A-15e. Grain Size Distribution for Core 10, Physical Sample.



Susquehanna, Core 10 Sample 5

Figure A-15f. Grain Size Distribution for Core 10, Physical Sample.

Erosion versus Depth



Figure B-1. Erosion versus depth for core 1. Colors indicate bed layers, symbols indicate applied shear stress.



Figure B-2. Erosion versus depth for core 2. Colors indicate bed layers, symbols indicate applied shear stress.



Figure B-3. Erosion versus depth for core 3. Colors indicate bed layers, symbols indicate applied shear stress.



Figure B-4. Erosion versus depth for core 4. Colors indicate bed layers, symbols indicate applied shear stress.

B-2



Figure B-5. Erosion versus depth for core 5. Colors indicate bed layers, symbols indicate applied shear stress.



Figure B-6. Erosion versus depth for core 6. Colors indicate bed layers, symbols indicate applied shear stress.



Figure B-7. Erosion versus depth for core 9. Colors indicate bed layers, symbols indicate applied shear stress.



Figure B-8. Erosion versus depth for core 10. Colors indicate bed layers, symbols indicate applied shear stress.

Erosion versus shear stress (Partheniades)

Table B-1. Cohesive Sediment Erosion Parameterization					
		Critical Shear (т _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)	
Layer ID	Depth (cm)	Ра	-	-	
Core01_L1	0-4	0.20	2.02E-02	1.14	
Core01_L2	5-10	0.40	2.89E-02	1.10	
Core01_L3	10-14	0.80	3.52E-02	0.96	



Figure B-9. Erosion versus applied shear stress for core 1, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-10. Erosion versus applied shear stress for core 1, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-11. Erosion versus applied shear stress for core 1, Layer 3. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-2. Cohesive Sediment Erosion Parameterization				
		Critical Shear (т _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)
Layer ID	Depth (cm)	Ра	-	-
Core02_L1	0-10	0.20	1.01E-01	1.05
Core02_L2	10-17	0.40	5.98E-02	1.52
Core02_L3	17-24	0.80	3.73E-02	1.36
Core02_L4	24-32	1.60	9.18E-02	0.92
Core02_L3&4	17-32	0.80	3.86E-02	0.92



Figure B-12. Erosion versus applied shear stress for core 2, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-13. Erosion versus applied shear stress for core 2, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-14. Erosion versus applied shear stress for core 2, Layer 3. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-15. Erosion versus applied shear stress for core 2, Layer 4. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-16. Erosion versus applied shear stress for core 2, Layer 3 and Layer 4. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-3. Cohesive Sediment Erosion Parameterization					
		Critical Shear (T _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)	
Layer ID	Depth (cm)	Ра	-	-	
Core03_L1	0-2.5	0.20	9.90E-03	0.98	
Core03_L2	2.5-22	0.80	8.08E-02	1.00	



Figure B-17. Erosion versus applied shear stress for core 3, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-18. Erosion versus applied shear stress for core 3, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-4. Cohesive Sediment Erosion Parameterization					
		Critical Shear (T _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)	
Layer ID	Depth (cm)	Ра	-	-	
Core04_L1	0-2	0.20	1.04E-02	1.21	
Core04_L2	2-11	0.80	3.23E-02	0.90	



Figure B-19. Erosion versus applied shear stress for core 4, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-20. Erosion versus applied shear stress for core 4, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-5. Cohesive Sediment Erosion Parameterization					
		Critical Shear (T _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)	
Layer ID	Depth (cm)	Ра	-	-	
Core05_L1	0-5	0.20	1.20E-02	1.04	
Core05_L2	5-12	0.78	2.17E-02	1.37	
Core05_L3	12-24	1.60	9.80E-02	0.99	



Figure B-21. Erosion versus applied shear stress for core 5, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-22. Erosion versus applied shear stress for core 5, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-23. Erosion versus applied shear stress for core 5, Layer 3. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-6. Cohesive Sediment Erosion Parameterization					
		Critical Shear (T _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)	
Layer ID	Depth (cm)	Ра	-	-	
Core06_L1	0-2	0.10	1.48E-02	0.90	
Core06_L2	2-14	1.60	3.31E-02	1.04	



Figure B-24. Erosion versus applied shear stress for core 6, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-25. Erosion versus applied shear stress for core 6, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-7. Cohesive Sediment Erosion Parameterization					
		Critical Shear (T _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)	
Layer ID	Depth (cm)	Ра	-	-	
Core09_L1	0-2	0.20	8.20E-03	1.41	
Core09_L2	2-9	1.52	2.32E-02	1.36	


Figure B-26. Erosion versus applied shear stress for core 9, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-27. Erosion versus applied shear stress for core 9, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-8. Cohesive Sediment Erosion Parameterization										
		Critical Shear (T _{cr})	Erosion Rate Constant (M)	Erosion Rate Ex- ponent (n)						
Layer ID	Depth (cm)	Ра	-	-						
Core10_L1	0-8	0.18	3.40E-02	1.31						
Core10_L2	8-16	1.14	1.70E-02	1.61						



Figure B-28. Erosion versus applied shear stress for core 10, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-29. Erosion versus applied shear stress for core 10, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Erosion versus shear stress (HEC-RAS fit to Partheniades)

Table B-9. Cohesive Sediment Erosion Parameterization for HEC-RAS											
	Depth	Shear ⁻ o	Shear Thresh- old Erosion Ra		n Rate	Mass Wasting Threshold		Mass Wasting Rate			
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft ² /hr	Ра	lb/ft ²	kg/m²/s	lb/ft ² /hr		
Core01_L1	0-4	0.2	0.0042	2.02E-02	14.9	1	0.0209	0.263	193.9		
Core01_L2	5-14	0.4	0.0084	3.24E-02	23.9	-	-	-	-		
Core01_L3	10-14	0.8	0.0167	3.39E-02	25.0	-	-	-	-		



Figure B-30. Erosion versus applied shear stress for core 1, Layer 1. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-31. Erosion versus applied shear stress for core 1, Layer 2. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-32. Erosion versus applied shear stress for core 1, Layer 3. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-10. Cohesive Sediment Erosion Parameterization for HEC-RAS											
	Depth (cm)	Shear o	Thresh- Id	Erosion Rate		Mass Wasting Threshold		Mass Wasting Rate			
Layer ID		Ра	lb/ft ²	kg/m²/s	lb/ft²/hr	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr		
Core02_L1	0-10	0.2	0.0042	1.04E-01	76.7	-	-	-	-		
Core02_L2	10-17	0.4	0.0084	6.32E-02	46.6	0.9	0.0188	0.323	238		
Core02_L3	17-24	0.8	0.0167	4.62E-02	34.1	-	-	-	-		
Core02_L4	24-32	1.6	0.0334	8.86E-02	65.3	-	-	-	-		
Core02_L3&4	17-32	0.8	0.0167	3.53E-02	26.0	-	-	-	-		



Figure B-33. Erosion versus applied shear stress for core 2, Layer 1. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-34. Erosion versus applied shear stress for core 2, Layer 2. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-35. Erosion versus applied shear stress for core 2, Layer 3. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-36. Erosion versus applied shear stress for core 2, Layer 4. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-37. Erosion versus applied shear stress for core 2, Layer 3 and Layer 4. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-11. Cohesive Sediment Erosion Parameterization for HEC-RAS											
Depth		Shear o	Thresh- Id	Erosio	n Rate	Mass \ Thre	Wasting shold	Mass W Ra	/asting ite		
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft ² /hr	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr		
Core03_L1	0-2.5	0.2	0.0042	9.60E-03	7.08	-	-	-	-		
Core03_L2	2.5-22	0.8	0.0167	8.07E-02	59.5	-	-	-	-		
Core03_L1&2	0-22	0.2	0.0042	1.09E-02	8.04	2	0.0418	0.237	175		



Figure B-38. Erosion versus applied shear stress for core 3, Layer 1. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-39. Erosion versus applied shear stress for core 3, Layer 2. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-40. Erosion versus applied shear stress for core 3, Layer 1 and Layer 2. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-12. Cohesive Sediment Erosion Parameterization for HEC-RAS											
	Depth	Shear Thresh- old		Erosion Rate		Mass Wasting Threshold		Mass Wasting Rate			
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr		
Core04_L1	0-2	0.2	0.0042	1.20E-02	8.85	0.8	0.0167	0.087	64.1		
Core04_L2	2-11	0.8	0.0167	2.82E-02	20.8	-	-	-	-		



Figure B-41. Erosion versus applied shear stress for core 4, Layer 1. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-42. Erosion versus applied shear stress for core 4, Layer 2. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-13. Cohesive Sediment Erosion Parameterization for HEC-RAS											
	Depth	Depth		Thresh- Id	Erosion Rate Three		Mass Wasting Threshold		Mass Wasting Rate		
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft ² /hr	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr		
Core05_L1	0-5	0.2	0.0042	1.28E-02	9.44	-	-	-	-		
Core05_L2	5-12	0.8	0.0167	2.22E-02	16.4	2	0.0418	0.125	92.2		
Core05_L3	12-24	1.6	0.0334	9.76E-02	72.0	-	-	-	-		



Figure B-43. Erosion versus applied shear stress for core 5, Layer 1. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-44. Erosion versus applied shear stress for core 5, Layer 2. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-45. Erosion versus applied shear stress for core 5, Layer 3. Colors indicate bed layers, Lines represent best-fit line to HEC-RAS implementation of Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-14. Cohesive Sediment Erosion Parameterization for HEC-RAS											
	Depth	Shear Thresh- old		Erosion Rate		Mass Wasting Threshold		Mass Wasting Rate			
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr		
Core06_L1	0-2	0.1	0.0021	1.32E-02	9.73	-	-	-	-		
Core06_L2	2-14	1.59	0.0332	3.41E-02	25.1	-	-	-	-		



Figure B-46. Erosion versus applied shear stress for core 6, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-47. Erosion versus applied shear stress for core 6, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-15. Cohesive Sediment Erosion Parameterization for HEC-RAS											
	Shear Thres old Depth		Thresh- Id	Erosion Rate		Mass Wasting Threshold		Mass Wasting Rate			
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr	Ра	lb/ft ²	kg/m²/s	lb/ft ² /hr		
Core09_L1	0-2	0.2	0.0042	1.25E-02	9.22	0.8	0.0167	0.102	75.2		
Core09_L2	2-9	1.58	0.033	3.43E-02	25.3	-	-	-	-		



Figure B-48. Erosion versus applied shear stress for core 9, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-49. Erosion versus applied shear stress for core 9, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.

Table B-16. Cohesive Sediment Erosion Parameterization for HEC-RAS										
	Depth	Shear ⁻ o	Thresh- Id	Erosion Rate		Mass Wasting Threshold		Mass Wasting Rate		
Layer ID	(cm)	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr	Ра	lb/ft ²	kg/m²/s	lb/ft²/hr	
Core10_L1	0-8	0.19	0.004	5.08E-02	37.5	-	-	-	-	
Core10_L2	8-16	1.19	0.0249	1.95E-02	14.4	2.8	0.0585	0.139	102	



Figure B-50. Erosion versus applied shear stress for core 10, Layer 1. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.



Figure B-51. Erosion versus applied shear stress for core 10, Layer 2. Colors indicate bed layers, Lines represent best-fit line to Partheniades' erosion function. Erosion equation parameters provided at top of figure.